



Membrane Permeability Threshold for Osmotic Power Plant Efficiency

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ARTICLE INFO:

Article history:

Received 2 August 2017

Accepted 23 August 2017

Available online 12 October 2017

Keywords:

Osmotic Energy,
Membranes,
Permeability,
Osmotic Pressure.

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ABSTRACT

In a context of ever-growing electricity consumption and need for less polluting sources of energy, salinity gradient power (SGP) based on osmosis is a promising technology. Salinity difference between two solutions separated by a semi-permeable membrane leads to the pressure increase. The aim of this study is to find the critical permeability threshold of a membrane for the dimensioning an osmotic power plant. Using Spiegler-Kedem equations, the various fluxes across the membrane have been calculated, and delivered power is explicitly derived in terms of system parameters. A necessary condition for economic viability is that its upper bound is larger than a critical threshold value below which osmotic power plant is not profitable. As it is directly proportional to membrane permeability, fixing the optimal membrane permeability value will in turn enable conceive more efficient membranes specifically made for osmotic energy production, as such membranes do not exist today.

JOURNAL OF CONTEMPORARY URBAN AFFAIRS (2017) 1(3), 49-53.

<https://doi.org/10.25034/ijcua.2018.3679>

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1. Introduction

The considerable and very fast growing energy consumption consecutive to the economic development of many countries is acutely raising the question of avoiding disastrous environmental consequences which could inevitably occur if only conventional fossil sources are used. To cope with such situation, a large effort has been oriented toward other sources such as less damaging renewable ones (Lewis, *et al.*, 2011; Kumar, *et al.*, 2011). Aside solar, wind, geothermal and hydraulic sources, they also include other less evident ones which may however represent interesting alternatives in specific situations.

Such is the osmotic power which is the process of converting the pressure differential between water with high salinity and water with lower or no salinity into hydraulic pressure (Loeb, 1975;

Mishra, 2013; Kho, 2010; The European Commission, 2004; Helfer, *et al.*, 2013; Skilhagen, *et al.*, 2012; Skilhagen, and Aaberg, 2012). The harnessing of this energy for conversion into power can be accomplished by means of Pressure Retarded Osmosis (PRO) (Kim, and Elimelech, 2013; Helfer, *et al.*, 2014; Wang, *et al.*, 2012). This technique uses a semipermeable membrane to separate a less concentrated solution, or solvent, (for example, fresh water) from a more concentrated and pressurized solution (for example sea water), allowing the solvent to pass to the concentrated solution side (Post, 2009). The additional volume increases the pressure on this side, which can be depressurized by a hydro-turbine to produce power and

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electricity (Kleiterp, 2012) .As seventy percent of Earth surface is covered with water, 97 percent of which is saltwater, the process created by mixing seawater with freshwater generates a resulting osmotic power which could serve as both renewable and consistent electricity source. While still in early stages, best estimates of the global production potential of osmotic power exceed 1,600 terawatt-hours, the equivalent of half of Europe entire energy demand. There are two primary sources for osmotic power: 1) natural occurrence where river water meets the sea water, and 2) merging two man-made water sources from processing plants

Both methods can be viable but in 1), seawater averages 40 grams of salt/ liter + River Water, less power is provided than in than 2), where brine (from desalination) averages 60 grams of salt/ liter + treated water. The higher the salinity, the more free energy can be extracted, and the more power can be generated. Today osmotic power is a promising renewable energy source (RES) provided conversion factor from pressure differential can be made large enough (Dinger, et al., 2012; Bræin, et al., 2010; Straub, et al., 2016). In the following, some elements on this question will be discussed in PRO case. In particular, the threshold value for permeability coefficient which characterizes membrane efficiency for viable economic application is determined.

2. Osmosis Pressure Representation

Potential osmotic pressure π , the maximum osmotic pressure in a solution separated from osmosed fluid by a selectively permeable membrane, is given by

$$\pi = CiRT \tag{1}$$

with π the potential osmotic pressure (Pa), C the solute molar concentration (mol m^{-3}), $R = 8,314 \text{ J. mol}^{-1} . \text{K}^{-1}$, T solution temperature ($^{\circ}\text{K}$), and I the particle number per entity. Given the solutions, D and F with respective osmotic pressures π_D and π_F , where D is draw solution (most concentrated), and F feed one (less concentrated), osmotic pressure difference $\Delta\pi = \pi_D - \pi_F$ between the two solutions is typically equal to 12 bars for water fluid, ie, 12.10^5 Pa . Let $\Delta P = P_D - P_F$ with P_D and P_F the pressures of solutions D and F. With Spiegler-Kedem [18] model flux equations can be integrated and one gets volume and solute fluxes J_v and J_s flowing through the membrane with pressure retarded osmosis

$$J_v = A(\sigma\Delta\pi - \Delta P) \quad ; \quad J_s = -(1 - E_m)^{-1}(J_v C_d E_m - C_i) \tag{2}$$

with J_v , J_s (m.s^{-1}) the volume and solute fluxes across the membrane, σ the solute reflection coefficient, $A(\text{m.Pa}^{-1} \text{ s}^{-1})$ the membrane fluid permeability, and $E_m = \exp - [(1 - \sigma) J_v L \omega^{-1}]$ with ω the solute permeability. Similarly in the support one gets

$$J_s = -(1 - E_s)^{-1}(J_v C_i E_s - C_f) \tag{3}$$

with C_d , C_i and C_f the solute concentration in the draw solution, at the barrier-layer/support interface, and in the feed solution respectively, and $E_s = \exp - [J_v \delta D_e^{-1}]$ with δ the support thickness. Equality of fluxes in the barrier layer and the support gives from (1,2,3) the non-dimensional equation

$$\alpha\{(1-\sigma)(1-E^{1-\sigma})^{-1} + E^{\rho}(1-E^{\rho})^{-1}\} = (1-r)(1-E^{\rho})^{-1} - \sigma \tag{4}$$

with $\alpha = 1 - C_i/C_d$, σ the solute reflection coefficient, $r = C_f/C_d$, $\rho = \delta\omega/D_e L$, δ the support thickness, L the barrier layer thickness, D_e the effective diffusion coefficient of the solute, $E = \exp - X$, $X = F(\sigma\alpha - \langle\Delta P\rangle)$, $F = ARTvC_dL/\omega$, v the salt stoichiometric coefficient and finally $\langle\Delta P\rangle = (P_d - P_f)/RTvC_d$. For a given dimensionless hydrostatic-pressure difference $\langle\Delta P\rangle$, (4) is a transcendental equation in α (dimensionless concentration difference across the barrier layer) which determines the operating conditions of the osmotic plant for a given set of system parameters.

3. Osmotic Power Plant Production

The basic energy production system is composed of a compression unit which delivers pressurized salted water injected in a chamber with a filtering membrane across which a flux of salted water J_s is crossing, see Figure 1.

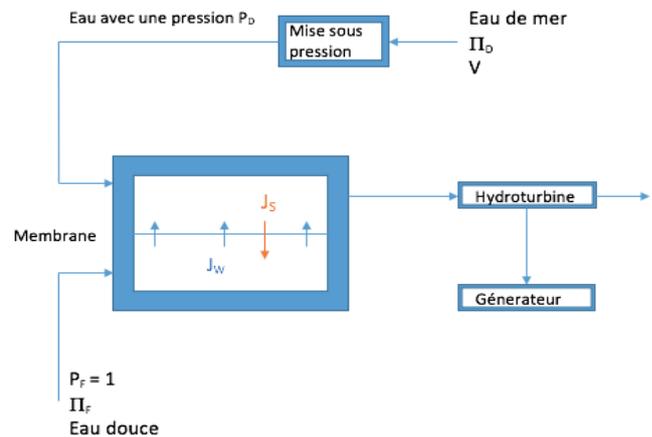


Figure 1. Sketch of Osmotic Plant Balance
 J_s is Salt Flux across the Membrane.

The power produced per surface unit of installed membrane is given $W = J_m \Delta P$ with W in Watts/ m^{-2} , or else in non-dimensional form

$$\langle W \rangle = W/A(RTvC_d)^2 = \langle\Delta P\rangle(\sigma\alpha - \langle\Delta P\rangle) \tag{5}$$

$\langle W \rangle$ is maximum when $\langle \Delta P \rangle = \sigma\alpha/2$ and is then equal to $\langle W \rangle = (\sigma\alpha)^2/4$. But this is not necessarily possible as α and $\langle \Delta P \rangle$ are also linked by (4) which imposes a constraint on system coefficients. One effectively gets for $z = \sigma\alpha$ the transcendental equation

$$z\{(1-\sigma)(1-E(z)^{1-\sigma})^{-1} + E(z)^\rho(1-E(z)^\rho)^{-1}\} = \sigma(1-r)(1-E(z)^\rho)^{-1} - \sigma^2 \quad (6)$$

with $E(z) = \exp(-5Fz)$ which relates “physical” z (concentration performance) to “technical” F (barrier quality). From this different limits can be evaluated for possible power output from the system (Yip, and Elimelech, 2012; Yip, and Elimelech, 2011; Lin *et al.*, 2014). However simple ones are directly obtained from (6) for $\langle W \rangle$. In the case of very large ρ for instance, (4) takes the very simple form

$$Y = -(\ln(1-x))/x \quad (7)$$

where $x = \alpha[1-r((1-\sigma)^{-1})]$ and $Y = \sigma(1-\sigma-r)F/2$. In definition interval $x \in [0,1]$, Y is monotonically increasing from 1 to $+\infty$, and normalized delivered power $\langle W \rangle = Kx^2$, with $K = \sigma^2/4[1-r((1-\sigma)^{-1})]^2$, varies monotonically between 0 and K , showing that larger $\langle W \rangle$ corresponds to larger x . More generally parametric dependence of power output W can be obtained from (6) to get best parameter range. When returning to dimensional expression, W is upper bounded by $W_{sup} = KA(RTvC_d)^2$, and a necessary condition for economic efficiency is that

$$W_{sup} = KA(RTvC_d)^2 \geq W_{crit} \quad (8)$$

where W_{crit} is the threshold value above which the osmotic plant is viable. W_{sup} is larger with larger draw concentration C_d , larger temperature T and larger A , which has to be determined to satisfy economic system efficiency demand, ie here $A \geq A_{crit} = 4W_{crit}\Delta\pi^2$. For usual figure of delivered power $W_d = 5Wm^{-2}$, and with typical $\Delta\pi = 12.10^5Pa$ for water, one gets, for instance, $A \geq A_{crit} = 1.38 mPa^{-1}s^{-1}$. More generally the variation of A_{crit} vs $\Delta\pi$, sees Figure 2, indicates for $\Delta\pi \in [6.10^5, 20.10^5]$ the “efficiency” interval $A \in [4.910^{-12}, 5.410^{-11}]$ which is still at technical limit today (Straub, *et al.*, 2016; Zhang, and Chung, 2013). To cope with these economic operating constraints, extension of simple osmotic barrier effect have been recently considered (Chou, *et al.*, 2013; Chou, *et al.*, 2012; Yip, *et al.*, 2010; Banchik, *et al.*, 2014; Mc Cutcheon, and Elimelech, 2007; Cath, *et al.*, 2013; Chen, *et al.*, 2016; She, *et al.*, 2016; Chou, *et al.*, 2013; Hickenbottom, *et al.*, 2016; Dechadilok, and Deen, 2006).

A coupled system with solar plant will be discussed elsewhere.

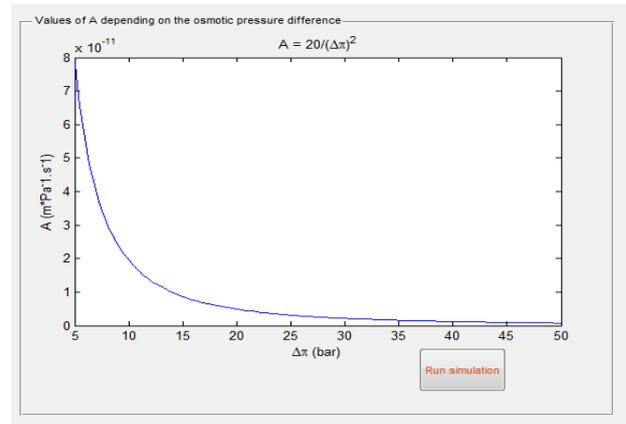


Figure 2 . Permeability Coefficient vs Osmotic Pressure Difference.

4. Conclusion

From analysis of equations representing osmotic physical phenomenon, it is shown that in Pressure Retarded Osmosis case, the harnessing of salinity-gradient energy taking place at the interface between waters of different salt concentration could provide an interesting and almost inexhaustible energy source if systems coefficients satisfy operating conditions which have been explicitly stated within Spiegler-Kedem model. However, even in optimum mode operating case, satisfaction of economic viability condition expressed by fixed specific membrane power output $W_{thres} \cong 5 Wm^{-2}$ is not always met. Aside theoretical research on optimizing system operating mode, this weakness is urging further study of membrane physical properties, such as porosity and tortuosity pore length, to design most efficient hydraulic permeability of the barrier layer.

Acknowledgments

The authors are very much indebted to ECE Paris School of Engineering for having provided the necessary setup for the development of the project, to Drs. S. Mouhali for advices during the research and Pr. M. Cotsaftis for help in the preparation of the manuscript.

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